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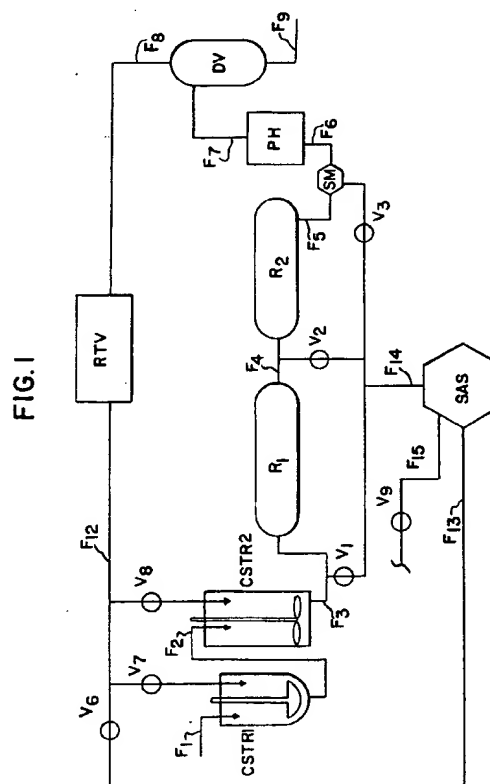
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54 **Apparatus for injecting solid insoluble additives into polymerization streams.**

57 Process and apparatus are disclosed for improved additive systems for polymerization processes, which improved systems comprise a slurry additive system having a high shear mixer for mixing a carrier fluid and solid and liquid additives and maintaining them in a suspension slurry prior to injecting them into the polymerization system.



FIELD OF THE INVENTION

This invention relates to the field of polymerizing mono-vinyl aromatic compounds and more particularly discloses methods and apparatus for adding thermally-sensitive and oxidation-sensitive additives and anti-oxidants to the reactants in a monovinylaromatic polymerization system prior to or during the polymerization process.

BACKGROUND OF THE INVENTION

Of all the thermoplastics manufactured today, probably the most versatile and most widely used class of materials is polymerized monovinyl aromatic compounds such as polystyrene, polymerized alpha-methyl styrene, and polymer of ring-substituted styrenes.

Virgin polystyrene manufactured by the polymerization of styrene monomer often requires the inclusion therein of additives such as pigments, stabilizers, anti-foaming agents, mold-release agents, plasticizers, and anti-oxidants. Plasticizers such as mineral oil and mold-release and stabilizer agents such as zinc stearate are necessary in the polymer to allow it to be formed in processing equipment into the final consumer products. Anti-oxidants such as Irganox 1076, a hindered phenol manufactured by Ciba-Geigy Corporation of Greensboro, North Carolina, are necessary to prevent the polymer from degrading with age and from exposure to ultra violet light from sources such as sunlight and artificial lighting.

As already mentioned, one of the most desirable, if not the most desirable, lubricant and mold-release agents added to polystyrene and other polymerized monovinyl aromatic compounds is zinc stearate. In conventional polymerization systems, zinc stearate is added to the process by first melting it in a closed heated vessel at 120° to 130°C and then pumping it into the polymerization system at the desired location. The problems with this approach are many.

First, the molten zinc stearates as well as other additives, oxidize easily at temperatures above their melting points, and must be completely shut off from any traces of air to prevent oxidation of the material, which causes yellow discoloration of the finished polymer. This is normally achieved by maintaining the headspace in the melting vessel filled with nitrogen.

Second, feeding problems often occur when trying to transport molten zinc stearate to the polymerization system. If any traces of air were allowed to leak in through the lines or fittings to the melt, the aforementioned oxidation will occur. Also, if the stearate supply piping were not maintained above the melt temperature of the stearate, the material would begin to solidify and precipitate out, clogging the lines or allowing solid chunks of the material into the polymerization process, adulterating the finished polymer.

SUMMARY OF THE INVENTION

The present invention discloses methods and apparatus for adding additives such as plasticizers, stabilizers, mold-release agents and anti-oxidants into polymerization processes, and more particularly discloses methods and apparatus for adding mineral oil, zinc stearate and hindered phenol compounds to polymerization systems by forming a slurry of the additives in an agitated vessel and injecting the slurry into the process at the desired location, or locations, at easily-controlled temperatures.

BRIEF DESCRIPTION OF THE DRAWINGS

Figure 1 is a schematic diagram of a typical monovinyl aromatic polymerization process illustrating the present invention in place therein.

Figure 2 is a schematic diagram of one embodiment of the slurry additive system for use in a polymerization process.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

Referring to the illustration of Figure 1, this is a schematic diagram of a typical high impact polystyrene (HIPS) manufacturing process. Such a process is more particularly described in US Patent No. 4,857,587 in the name of Sosa et al, entitled "Continuous Process Including Recycle Stream Treatment for the Production of High Impact Polystyrene", which patent is hereby incorporated by reference in its entirety into the present application. In a typical high impact polystyrene process, such as that illustrated in Figure 1, refined styrene monomer feed is fed through flow line F1 into a stirred tank reactor (CSTR1) which is a continuous stirred tank reactor. Styrene, polybutadiene, a free-radical initiator, and additional components such as solvents, anti-oxidants, dyes, and other additives are fed into the reactor through feed line F1. As used herein, the term "styrene" includes a variety of substituted styrenes, such as alpha-methyl styrene, ring-substituted styrenes, such as p-methylstyrene and p-chlorostyrene, as well as unsubstituted styrene. Typically, the mixture in polymerization reactor CSTR1 will comprise about 75 to 99% by weight refined styrene, about 1 to 15% by weight polybutadiene, and the remainder being free-radical initiator and additional components.

The feed components fed through line F1 are stirred in CSTR1 and reaction between the components is initiated therein. The components are then fed through flow line F2 into a second continuous stirred tank reactor CSTR2 for additional reaction and agitation by stirring. From there the HIPS components are transferred through flow line F3 into an initial polymerization reactor R1. A pair of reactors R1, and

R2, each comprising horizontal polymerization reactors may be used for the total polymerization process of the HIPS material. The polymerized styrene/butadiene mixture exits reactor R2 and passes through flowline F5 to an optional static mixer SM and from there through flow line F6 into a preheater PH. From the preheater the polymerized product flows through line F7 into a devolatilizer DV where volatile components are transferred through line F8 to the recycle treatment vessel RTV. The finished HIPS material then exits DV through line F9 to the product finishing line where it may be pelletized or put into other transportable forms. The volatile elements removed in the devolatilizer DV are then passed through vessel RTV which usually comprises a filter bed such as clay to remove the acid components from the recycle stream. The refined recycle stream then moves through line F12 and may be recycled into the CSTR1 or CSTR2.

The description given above is that of a typical high impact polystyrene manufacturing system described from a schematic or flow diagram viewpoint. The present invention involves the use of a slurry additive system for adding components such as antioxidants, stabilizers, mold-release agents, and other desirable compounds. The slurry additive system is more particularly described in Figure 2 and is designated schematically at SAS with a feed input line F13 and a slurry supply line F14. Line F13, by means of manipulation of valves V6, V7, and V8, is arranged to provide recycled monomer from the RTV into the slurry additive system as a carrier for the additive to be injected into the polymerization reactor system R1-R2.

The recycle stream entering the SAS vessel through F13 is slurried with the desirable additive, such as the previously mentioned zinc stearate and hindered phenol additives, to be injected into the polymerization system by manipulating valves V1 through V3. Injection of the additive slurry may be directed at any point in the polymerization process: by closing all valves except V1 the additive slurry may be injected prior to the polymerization reactor R1. Likewise, by opening valves V2, and V3, and closing all the other valves, the injection points may be moved to the various locations shown in the drawings. The opening of valve V3 and closing of valves V1 and V2 introduces the additive slurry into the system after the final reactor vessel R2.

In this case, the optional static mixer SM must be utilized to thoroughly compound the additive slurry into the polymer stream. As previously mentioned, the static mixer SM is an optional element and is intended for the particular embodiment wherein the additive slurry is injected between the reactor system R1-R2 and the preheater PH. It is contemplated that if the injection point is at any other point in the system prior to reactor R2 then the static mixer SM will not be necessary and

the output of R2 can be routed around the static mixer SM and into the preheater PH.

Alternatively, if it is undesirable to utilize the recycle stream for a carrier material in the SAS, an alternate carrier fluid may be introduced into the slurry system through feed line F15 from an independent carrier material source (not shown). In one particular embodiment such a carrier material could be mineral oil which is often used as a plasticizer in polystyrene materials. In such a case, it would only be necessary to close valve V6 and open valves V7 and V8 as well as valve V9.

Referring now to Figure 2, there is illustrated a detailed schematic drawing of the slurry additive system SAS of Figure 1. The SAS comprises a high shear mixer HSM located in a mixing vessel MV and having the feed inlet line F13 flowing thereto. A zinc stearate supply ZS, which is added as a solid is indicated in the dashed line next to flow line F13. Zinc stearate may be added to the vessel by any conventional means such as a vessel hatch or gear pump or other means for adding solid material into a closed vessel. The carrier fluid entering line F13, which as previously mentioned can be either mineral oil or the recycle stream from the devolatilizer DV, which primarily consists of about 80 to 90% styrene monomer, 5 to 10% ethylbenzene, and 5 to 10% xylenes, toluenes, and propylbenzene, is added to the agitator MV along with zinc stearate from a ZS supply and subjected to high shear through the action of the high shear mixer. This forms a finely divided slurry of zinc stearate in the carrier fluid which is then pumped through volumetric slurry pump SP and out flow line F16. A mass controller MC is located in flow line F16 and a recycle loop RL is branched off of line F16 upstream mass control of MC and feeds back into vessel MV. This type of system is commonly known as a "pump-around" system. Thus the action of mass control MC, which may be a conventionally known valving system, allows a constant control of the feed amounts through line F14 to the polymerization system.

Any slurry that is not transported through line F14 is directed through return line RL back into the agitation of the high shear mixer HSM in vessel MV. This maintains a constant and consistent slurry of the zinc stearate in the carrier fluid and prevents settling out of the solids in the suspension. By controlling the amount of zinc stearate added to the mixing vessel MV and/or controlling the amount of recycle fluid, or alternate carrier fluid such as mineral oil, being added through lines F13 and F15, the amount of additive slurry entering the polymerization system through flow line F14 can be very precisely controlled. Conventional ratios of the slurry additive material are known to those skilled in the art and can be adjusted precisely through the use of mass controller MC and slurry pump SP. Temperature of the slurry is maintained at a desirable constant value by the utilization

of heat exchanger HEX located in return line RL. In one preferred embodiment the temperature was maintained at about 70°F.

In addition to the placement of zinc stearate ZS into vessel MV, other additives can clearly be placed in the vessel to be slurried with the carrier fluid and the zinc stearate ZS. Such materials include those previously mentioned such as hindered phenols, anti-oxidants, solvents, initiators, and other such additives. The addition of other additives to the mixing vessel MV is indicated by a second dashed line designated at AA in Figure 2. As another alternative, the carrier fluid for the slurry may be made up of virgin styrene monomer diverted from feedline F1, or can be a mixture of virgin monomer and recycle stream fluid, as well as other solvents compatible with the process, such as ethylbenzene. In addition, the high shear mixer may be utilized to disperse insoluble liquids in the chosen carrier fluid in place of or in addition to insoluble solids.

OPERATION OF THE PREFERRED EMBODIMENT

In typical operation, the slurry additive system SAS as illustrated more precisely in Figure 2, is supplied with a carrier fluid such as a virgin styrene monomer, recycle styrene stream, or optionally, a mineral oil plasticizer, and one or more solid additives such as zinc stearate and anti-oxidants are placed in solid form into the closed vessel. There they are subjected to high shear and converted into a very finely divided suspension or slurry which is maintained by the constant action of a high shear mixer and a pump-around system. As the additives are needed, the slurry is pumped through a mass-controller into the polymerization system at any point prior to, in the middle of, or at the downstream end of the polystyrene polymerization reactor system. By utilizing the present invention, the need for heated zinc stearate vessels with nitrogen atmospheres are eliminated as well as the need for heated flow lines to prevent solidification of additives such as zinc stearate. The present invention provides a simple yet efficient means for injecting solid additives in a finely divided state into the styrene polymerization/copolymerization system as illustrated in Figure 1. By controlling the amounts of solids added into the high shear mixer, slurries of known composition can be precisely obtained and injected into the polymerization system, very closely controlling the amount of additives and obtaining a fine, even distribution in the polymerizing styrene.

It should also be noted that the optional heat exchanger HEX on line RL keeps the slurry at the desired temperature or within a desirable temperature range. There is no need for a nitrogen atmosphere in the mixing vessel since it is a closed vessel and the head-space is completely filled with the vapors generated from the recycle stream carrier fluid, but a nit-

rogen atmosphere can be utilized if desirable.

One particular additive utilized in styrene polymerization and added by the slurry additive system is solid zinc stearate. The agitation vessel MV was designed to maintain the particle size of the zinc stearate to less than 200 microns. The slurry was delivered to the polymerization process utilizing a volumetric pump SP to precisely control the concentration of the additive. The concentration of additives was adjusted to maintain proper viscosity, for example, approximately ten weight percent zinc stearate and ten weight percent Irganox 1076 were dispersed and added to the slurry system. If the soluble anti-oxidant Irganox were not to be utilized, then higher levels of zinc stearate could be used to maintain the viscosity. Irganox 1076 is soluble in styrene and thereby increases the viscosity of the solution. It was also found that by adding the anti-oxidant and other additives late in the process, i.e. for example, at the static mixer location, improved properties in the finished product could be obtained.

In summary, the slurry addition system is utilized to add heat-sensitive additives and additives that can possibly interfere in the early stages of the process into a monovinyl aromatic polymerization system.

Although a specific preferred embodiment of the present invention has been described in the detailed description and drawings above, the description is not intended to limit the invention to the particular forms or embodiments disclosed therein since they are to be recognized as illustrative rather than restrictive, and it would be obvious to those skilled in the art that the invention is not so limited. For example, instead of using the present system to slurry solid insoluble additives in a carrier fluid, the system could be utilized to add commercially available preformed emulsions or dispersions, such as a silicon oil/water and zinc stearate/mineral oil, by insuring that "settling-out" does not occur in these formulations. It is also contemplated that the present invention can be utilized successfully in polymerizing monomers other than monovinyl aromatics, such as ethylene, propylene, polyesters, and others. Thus, the invention is declared to cover all changes and modifications of the specific examples of the invention herein disclosed for purposes of illustration which do not constitute a departure from the spirit of the invention.

Claims

1. In a process for polymerizing organic compounds in which liquid and solid soluble and insoluble additives comprising plasticizers, stabilizers, lubricants, and anti-oxidants are added to the compounds prior to, during, or after polymerization; the improvement consisting in the process of adding said additives, said process comprising

the steps of:

- a) supplying at least one insoluble additive to a high-shear mixer;
 - b) supplying a carrier fluid to said high-shear mixer;
 - c) subjecting said carrier fluid and said additive to high shear mixing thereby forming a finely divided substantially homogeneous slurry of additive particles in said carrier fluid; and
 - d) injecting said slurry into said compounds in desirable amounts.
2. The process of claim 1 further comprising the steps of:
 - e) continuously subjecting said carrier fluid and said additive to high shear mixing; and,
 - f) pumping any excess slurry from said mixer through a pump-around loop, back into said mixer.
 3. The process of claim 1 wherein said additive comprises zinc stearate.
 4. The process of claim 1 wherein said additive comprises zinc stearate and said carrier fluid comprises mineral oil.
 5. The process of claim 4 wherein a substantial majority of said additive particles are sheared to a size of less than about 200 microns.
 6. The process of claim 5 wherein said additives further comprise an anti-oxidant.
 7. The process of claim 6 wherein said anti-oxidant consists essentially of a hindered phenol.
 8. The process of claim 2 further comprising the step of flowing said homogenous slurry through a heat exchanger in said pump-around loop and thereby maintaining the temperature of said slurry within a predetermined desirable range.
 9. The process of claim 4 further comprising the step of adding virgin unreacted organic monomer from said polymerizing process into said high-shear mixer.
 10. The process of claim 2 wherein said additive and said carrier fluid comprise a previously-prepared liquid/solid dispersion.
 11. The process of claim 2 wherein said additive and said carrier fluid comprise a previously-prepared liquid/solid emulsion.
 12. A process for adding additives to a polymerization

system, said process comprising:

- a) delivering at least one additive into a mixer;
 - b) delivering a carrier fluid into said mixer with said additive;
 - c) shearing said additive into finely-divided particles in said mixer, and forming a slurry of said particles in said carrier fluid;
 - d) maintaining said slurry by continuous pumping thereof to prevent settling of said particles out of said fluid; and,
 - e) injecting measured, desired amounts of said slurry into a polymerization process.
13. The process of claim 12 wherein said additive is sheared into relatively evenly-sized particles, a substantial percentage of which are below about 200 microns in size.
 14. The process of claim 12 wherein said additive comprises zinc stearate and said carrier fluid comprises mineral oil.
 15. The process of claim 14 wherein said additive further comprises anti-oxidants consisting essentially of hindered phenols.
 16. Apparatus for adding additives to a polymerization process, said apparatus comprising:
 - a mixing vessel adapted to divide an additive into evenly-sized, finely-divided particles;
 - an inlet flow line arranged to provide carrier fluid into said mixing vessel;
 - an entry port in said vessel for receiving additive materials;
 - an exit port connected to a flow line, adapted to transmit a slurry from said vessel; and,
 - a flow control and measurement system connected to said exit port flow line arranged to precisely measure and control the amount of said slurry flowing thereout.
 17. The mixing apparatus of claim 16 wherein said vessel comprises a high shear mixer arranged to divide additives into particles, a substantial percentage of which are below about 200 microns in size, and further adapted to mix said particles with said carrier fluid and form and maintain a slurry thereof.
 18. The mixing apparatus of claim 17 wherein said flow control and measurement system comprises a volumetric pump and a mass controller, connected in series.
 19. The mixing apparatus of claim 18 wherein said flow control and measurement system further comprises a pump-around loop leading back into said mixing vessel from a point between said

pump and said controller.

20. The mixing apparatus of claim 19 further comprising a heat exchanger arranged to maintain the slurry in said mixing vessel at a desirable temperature within a predetermined desirable range.

21. The mixing apparatus of claim 20 wherein said heat exchanger is located in said pump-around loop.

22. In a polymerization reactor system wherein virgin monomer feedstock is polymerized into a polymeric product containing desirable additives, the improvement consisting of a slurry additive system comprising:

a high-shear mixing vessel adapted to divide an additive material into evenly-sized, finely-divided particles;

an inlet flow line arranged to transmit a fluid into said mixing vessel;

an entry port in said vessel for receiving additive materials;

an exit port in one end of said vessel connected to a slurry supply line leading to said polymerization reactor system;

a flow control and measurement assembly in said slurry supply line arranged to measure and control the amount of slurry flowing therethrough; and,

a pump-around loop consisting of a flow line leading from said exit port back into an opposite end of said vessel.

23. The slurry system of claim 22 further comprising a heat exchanger in said system arranged to maintain the slurry in said mixing vessel within a desirable temperature range.

24. The slurry additive system of claim 22 wherein said polymerization reactor system has a recycle stream flowline for recycling unreacted monomer from the output of said reactor system back into the system, the improvement further comprising a recycle supply line from said recycle stream flowline into said mixing vessel.

25. The slurry additive system of claim 22 wherein said polymerization reactor system has a virgin monomer supply line leading thereinto and said improvement further comprises a flow line from said monomer supply line into said mixing vessel.

26. The slurry additive system of claim 22 wherein said inlet flowline is connected to said entry port for supplying previously prepared emulsions and dispersions into said mixing vessel.

27. The slurry additive system of claim 22 wherein said inlet flowline enters said mixing vessel at a point separate from said entry port; said inlet flowline is adapted for injecting a carrier fluid into said mixing vessel; and, said entry port is adapted to admit solid and liquid additives into said mixing vessel.

28. In a process for polymerizing compounds in which soluble and insoluble liquid and solid additives, comprising plasticizers, lubricants, stabilizers, anti-oxidants, and mold-release agents, are added to the compounds prior to, during, or after polymerization, and in which unpolymerized monomer and other products are recycled from a point at or near the downstream end of said polymerization process back to a point at or near the upstream end of said process; the improvement consisting in the process of adding at least one insoluble additive to said polymerization process, said adding process comprising the steps of:

a) supplying at least one insoluble additive to a high-shear mixer;

b) flowing at least a portion of said recycled stream containing monomer from said polymerization process into said mixer;

c) subjecting said insoluble additive to sufficient shear to divide it into fine particles and thereby form a substantially homogeneous slurry of said particles in said recycled monomer stream; and,

d) injecting desirable quantities of said slurry into said compounds.

29. The process of claim 28 further comprising the steps of:

e) continuously subjecting said insoluble additive and said recycled monomer stream to high shear mixing; and,

f) pumping any excess slurry from said mixer through a pump-around loop back into said mixer to prevent settling of the solids in said slurry.

30. The process of claim 28 wherein said compounds are monovinylaromatics and said insoluble additive comprises zinc stearate.

31. The process of claim 28 wherein said compounds are monovinylaromatics and said additives comprise an insoluble zinc stearate and a soluble hindered phenol anti-oxidant, which anti-oxidant is substantially soluble in monovinylaromatic monomer.

32. The process of claim 31 wherein a substantial majority of said insoluble particles are sheared to

- a size of less than about 200 microns.
33. A process for adding soluble and insoluble additives to a polymerization system, said process comprising:
- a) delivering at least one insoluble additive into a mixer;
 - b) delivering a stream containing unreacted monovinylaromatic monomer to said mixer;
 - c) shearing said additive into finely-divided particles in said mixer, and forming a substantially homogeneous slurry of said particles in said streams containing monomer;
 - d) maintaining said homogeneous slurry by preventing settling-out of said particles; and,
 - e) injecting measured desired amounts of said slurry into a polymerization process.
34. The process of claim 33 wherein at least a portion of said unreacted monomer is supplied from a recycle stream of a polymerization process.
35. The process of claim 33 wherein said additive is sheared into relatively even-sized particles, a substantial portion of which are below about 200 microns in size.
36. The process of claim 33 wherein said polymerization process is monovinylaromatics and said insoluble additive comprises solid zinc stearate.
37. The process of claim 33 further comprising the step of adding to said mixer a desirable amount of additive soluble in the monomer being polymerized.
38. The process of claim 37 wherein said polymerization process is monovinylaromatics, said solid insoluble additive is zinc stearate, and said soluble additive is a hindered phenol anti-oxidant.
39. The process of claim 33 further comprising the step of flowing said homogeneous slurry through a heat exchanger and thereby maintaining the temperature of said slurry within a predetermined desirable range.
40. A process for adding a prepared emulsion into a polymerization system, said process comprising:
- a) delivering said prepared emulsion into a mixer;
 - b) applying shear to said emulsion in said mixer, thereby maintaining said emulsion in a substantially homogeneous state; and
 - c) injecting measured desired amounts of said emulsions from said mixer into a polymerization process.
41. The process of claim 40 further comprising the step of adding to said mixer a stream of unreacted monomer from said polymerization system.
42. The process of claim 40 wherein said emulsion comprises silicon oil and water.
43. A process for adding a prepared dispersion into a polymerization system, said process comprising:
- a) delivering said prepared dispersion into a mixer;
 - b) applying shear to said dispersion in said mixer;
 - c) thereby maintaining said dispersion in a substantially homogeneous state; and,
 - d) injecting measured desired amounts of said dispersion from said mixer into a polymerization system.
44. The process of claim 43 wherein said dispersion comprises zinc stearate in mineral oil.
45. The process of claim 43 further comprising the step of forming a substantially homogeneous slurry by adding to said mixer a stream of unreacted monomer from said polymerization system.
46. The process of claim 45 wherein said dispersion comprises zinc stearate in mineral oil.
47. The process of claim 46 further comprising the step of flowing said slurry through a heat exchanger and thereby maintaining the temperature of said slurry within a predetermined desirable range.

FIG. 1

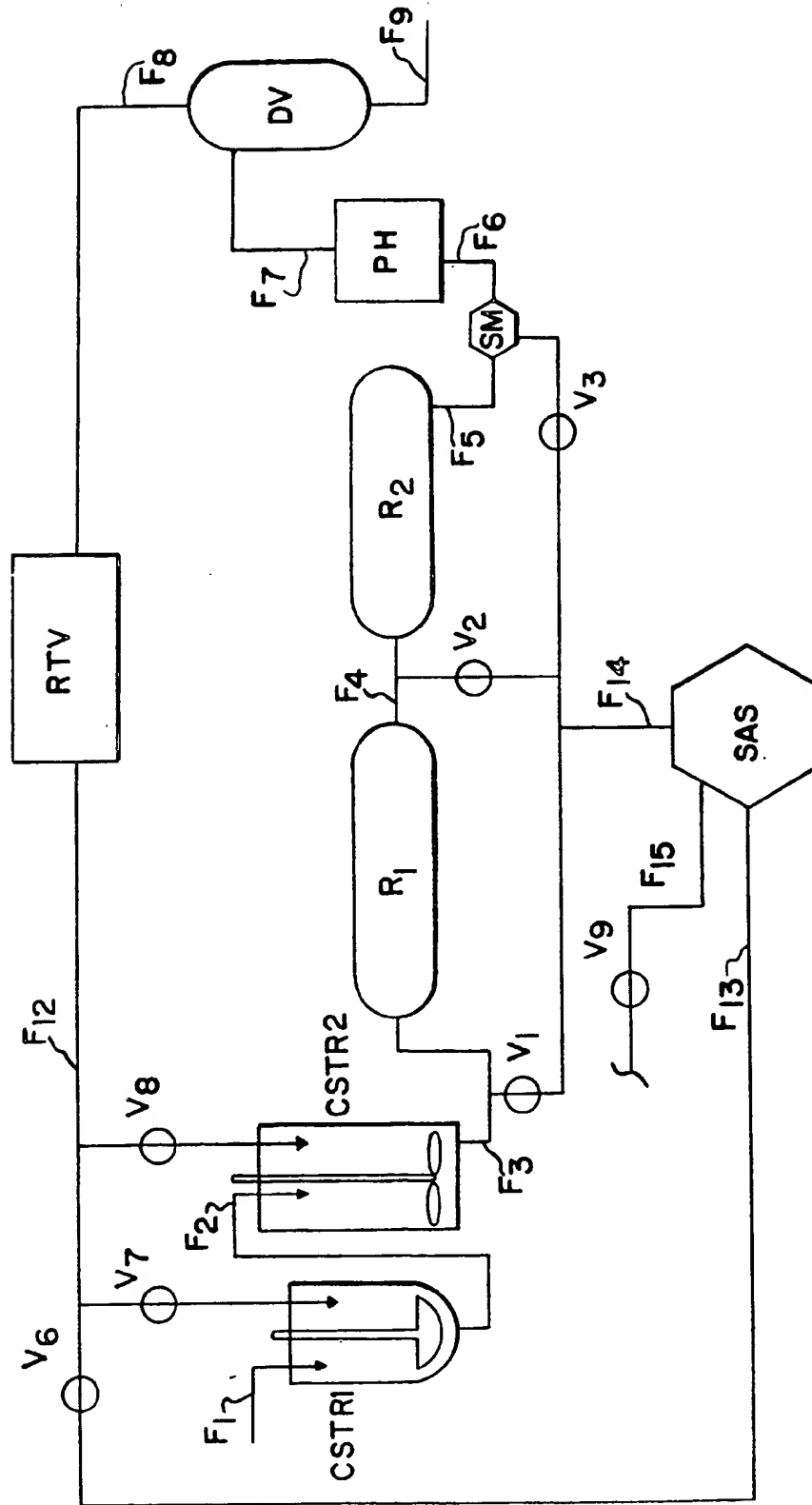
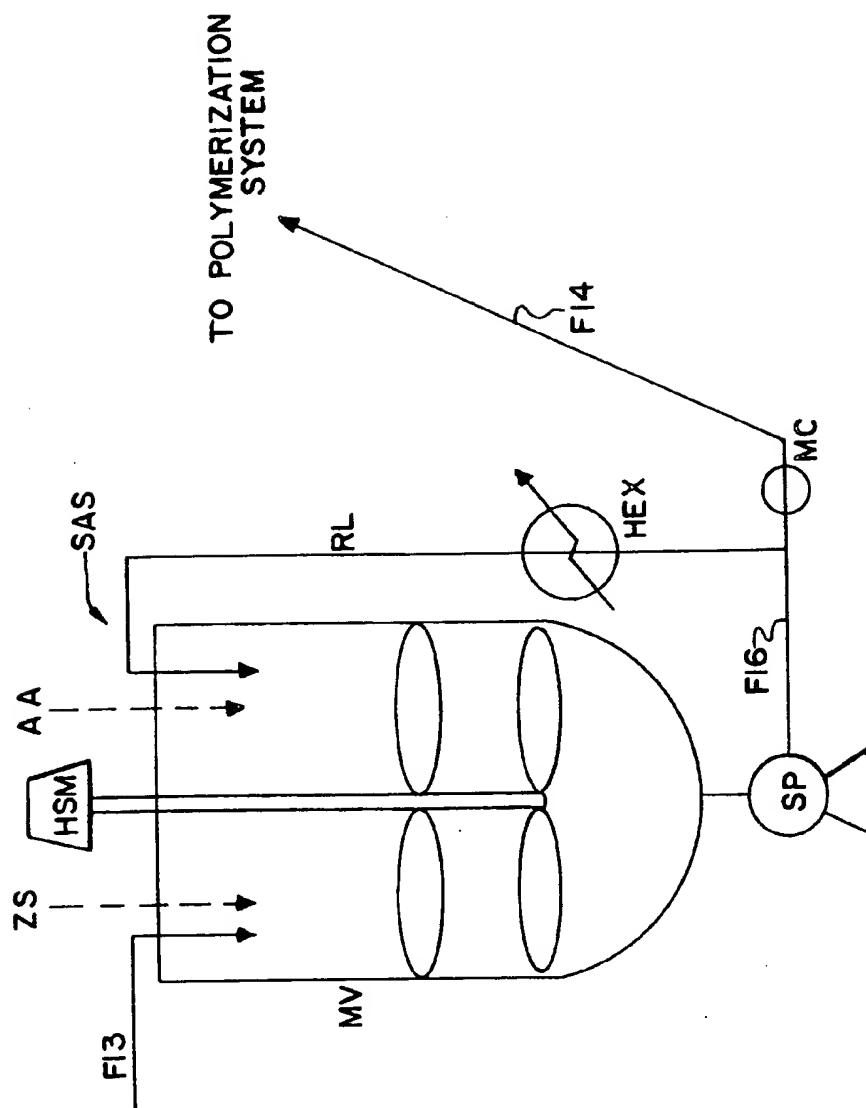


FIG. 2





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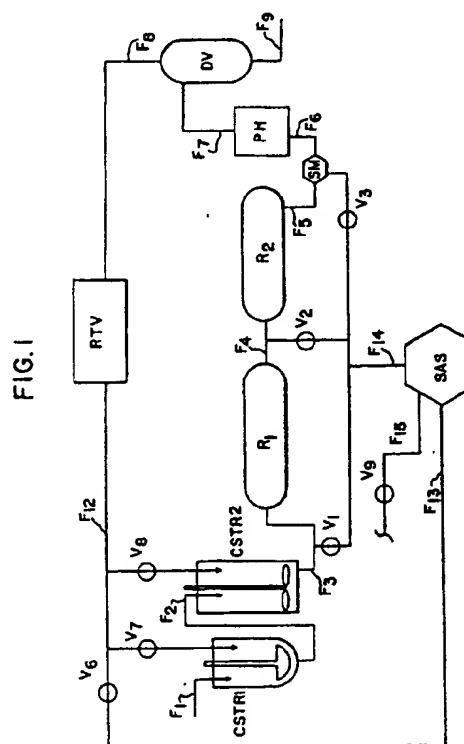
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EUROPEAN SEARCH REPORT

Application Number

EP 91 87 0189

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int. Cl.5)
A	GB-A-1 073 456 (I.C.I.) * claims 1,5 *	1	C08F2/44 C08F12/00 B01F3/12
A	EP-A-0 100 793 (DOW CHEMICAL RHEINWERK GMBH) -----		
			TECHNICAL FIELDS SEARCHED (Int. Cl.5)
			B01F C08F
The present search report has been drawn up for all claims			
Place of search THE HAGUE		Date of completion of the search 10 DECEMBER 1992	Examiner CAUWENBERG C.L.
<p>CATEGORY OF CITED DOCUMENTS</p> <p>X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document</p> <p>T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons A : member of the same patent family, corresponding document</p>			

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